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## A novel method to reduce differential crosstalk in a high-speed channel

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#### Outline

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- Theory and simulation result
  - Edge-coupled vias
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  - Broadside-coupled vias with offset
- Measurement
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#### Introduction

- Highspeed channel
  - Communication channel data rate is exponentially increasing to meet industry and consumer demand
- High density connection, crosstalk an issue
  - Connector and via crosstalk have become big contributors to total channel crosstalk due to their inherent large number of microwave transitions in order to support mechanical spec/tolerance/robustness
  - There exists situations where designing for impedance control degrades crosstalk, and so xtalk becomes even more of an issue

#### Introduction

- How crosstalk was handled in the past (isolation, cap/inductance control and polarity swapping)
  - Capacitive coupling can be controlled by varying  $\epsilon_r$  and inductive coupling by varying the radius of a wire/pin/via
  - Complexity on capacitance and inductance control, especially in PCB material
  - Polarity swapping adds complexity to routing
  - Relying too much on isolation (spacing) will consume valuable real estate on PCB
  - Relying too much on ground vias to contain crosstalk can take up PCB space and populate power planes with antipads

#### **Motivation**

- Adjusting individual single-ended terms to achieve desired differential crosstalk (either minimum within a component or desired magnitude and polarity in each component to have minimum in an entire channel)
  - Reduction in crosstalk NEXT/FEXT at component level
  - Reduction in FEXT by cascading multiple components with adjusted individual single-ended terms of components to provide opposite characteristic of each



#### Analyzing crosstalk in time domain

 Viewing crosstalk in time domain gives valuable information that one cannot immediately perceive from frequency domain response Single ended terms



#### **Edge-coupled**

- Single ended and differential crosstalk of edge-coupled vias in time-domain
- Applies to connector pins



#### Broadside coupled

 Single ended and differential crosstalk of broadside-coupled vias in timedomain



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#### Broadside coupling with offset

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- Single ended and differential crosstalk of broadside-coupled vias with an offset
- An optimum offset can significantly reduce differential crosstalk



#### Measurement result

- 1. Broadside-coupled vias with offset
- 2. Broadside via and edge-coupled via transitions
- 3. via-connector-via



Image: bit with the second	Test structure PCB stack up															
Image: Second				Desig								ack up Actual stack		ack up		
g1   g1   4 mils   3.2 mils   3.44     4.0 mils   3.66   4.6 mils   3.28     12 mils   12 mils   4.6 mils   3.28     14 mils   0.2   0.2   52   52     11 mtar differential pair via pitch   0.7   1.27   52   53     11 mter differential pair via pad Φ   0.45   0.45   53     11 mter differential pair via pad Φ   0.45   0.45   6     12 mils   5.8 mils   3.44     4.0 mils   3.66   3.66     12 mils   6 mils   5.8 mils   3.44     4.0 mils   3.66   3.66   3.66     12 mils   5.8 mils   3.44   3.66     14 mils   0.65   83   83   84     15 0.655   0.65   84   84   12 mils   4.0 mils   3.66     12 mils   12 mils   4 mils   3.2 mils   3.44     10 mils   3.66   3.28   3.44   3.44     10 mils   0.65   12 mils   12 mils   14 mils   3.66			То	n (s1) 📕	_					_		Laminate	٤r	Laminate	٤r	
Image: basic bas				σ1				Bac		<b>-</b>		4 mils		3.2 mils	3.44	
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Ex 1 and 2   Example 3   g2   g								d	rill			12 mils		4.6 mils	3.28	
Ex 1 and 2     Example 3     g2     6 mils     3.7     5.8 mils     3.44       Intra differential pair via pitch     0.7     1.27     3     6 mils     6 mils     8.0 mils     3.66       Inter differential pair via pad Φ     0.45     0.45     8     6 mils     5.8 mils     3.44       Sig. layer via pad Φ     0.45     0.45     8     8     3.44       Back     6 mils     6 mils     5.8 mils     3.44       Mitra differential pair pitch     NA     1.5     8						F	ŀ	7		<b>.</b>				4.0 mils	3.66	
Via drill Φ   0.2   0.2		Ex 1 and 2	Example 3	g2 s2 s3 g3 g4	11				I.		6 mils		5.8 mils	3 11		
Intra differential pair via pitch     0.7     1.27       Inter differential pair pitch     NA     1.5       Sig. layer via pad Φ     0.45     0.45       Via depth     1.5     0.65       Differential antipad Φ     0.6     NA       g4     g4     g4       Bottom (s4)     S0     S1       Differential antipad Φ     NA     0.91	Via drill Φ	0.2	0.2				41-		Ŀ			0 11115	3.7	5.6 11115	5.44	
Inter differential pair pitch     NA     1.5     53     a     b     a	Intra differential pair via pitch	0.7	1.27									6 mils		8.0 mils	3.66	
Sig. layer via pad Φ   0.45   0.45   93   84   86   84   4.0 mils   3.66     Via depth   1.5   0.65   6   6   6   12 mils   4.0 mils   3.28     Differential antipad Φ   0.6   NA   g4   g4   6   4 mils   3.28     Bottom (s4)   Bottom (s4)   Total thickness   50 mile   51 2 mile	Inter differential pair pitch	NA	1.5		╢				L			6 mils		5.8 mils	3.44	
Via depth     1.5     0.65     Back drill     12 mils     12 mils     4.0 mils     3.28       Differential antipad Φ     0.6     NA     g4     64     6711     12 mils     12 mils     4.0 mils     3.28       Antipad Φ     NA     0.91     g4     g4     64     64     12 mils     4 mils     3.28       Bottom (s4)     g4	Sig. layer via pad Φ	0.45	0.45			F.		- 1	L	•		12 mils		4.0 mile	2.00	
Differential antipad Φ     0.6     NA     g4     6     6     6     6     6     7     4.6 mils     3.28     4.0 mils     3.66     3.66     3.66     3.44	Via depth	1.5	0.65				Back							4.0 mils	3.00	
Antipad Φ NA 0.91 g4 </th <th>Differential antipad Φ</th> <th>0.6</th> <th>NA</th> <th></th> <th>um</th> <th></th> <th>I</th> <th></th> <th>4.0 mils</th> <th>3.28</th> <th></th>	Differential antipad Φ	0.6	NA				um		I					4.0 mils	3.28	
Bottom (s4) Total thickness 50 mile 51.2 mile	Antipad Φ	NA	0.91					-		•		4 mile		4.0 mile	2.44	
	•		Botto	m (s4)						•	otal thickness	4 mils		5.2 mils	5.44	









NEXT frequency domain







• FEXT frequency domain



#### Edge/broadside-coupled vias cascaded

- FEXT reduction through multiple components
- Need to analyze and adjust polarity of FEXT of each component to enable cancellation
- Proof of concept using edge-coupled and broadside-coupled vias in series



#### Edge/broadside-coupled vias cascaded

• Time domain response



#### Edge/broadside-coupled vias cascaded

Frequency domain response



#### Via-Connector-Via (simulation)



#### Via-Connector-Via

• Several tuning variables are available in designing proper polarity and magnitude of via design to reduce FEXT of the connector



#### Via-Connector-Via (simulation)

Offset of inter-differential pair vias varied to determine favorable FEXT cancellation value for the via design



#### Via-Connector-Via (simulation)

- Via design cascaded with connector model
- Improvement seen in both time and frequency domain



#### Via-Connector-Via (measurement)

- Measurement shows that cancellation indeed occurs
- Time domain data indicates that connector FEXT was over compensated and there is space for improvement



#### Via-Connector-Via

- ICR using 5 FEXT aggressors
- Improvement observed over wide frequency range





#### Conclusion

- Differential crosstalk reduction technique was investigated
- Polarity of crosstalk was explored using edge-coupled and broadside coupled PCB vias
- Crosstalk reduction within a component was demonstrated using vias that are broadside-coupled with an optimum offset
- Crosstalk reduction through multiple components was demonstrated using via-connector-via transitions



# Thank you!

